

Lecture 5: System Responses (Cont'd) and Stability

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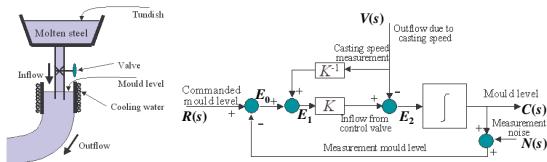
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Outline of this lecture

- An exercise from Lab 1
- Review of Lecture 4
- System responses
- Stability

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An exercise from Lab 1



- What is the relationship between the output $C(s)$ and the three inputs $R(s)$, $V(s)$, and $N(s)$?

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Review of Lecture 4

- What are the forced response, steady state response, natural response, transient response in the step response of a first-order system?

$$G(s) = \frac{C(s)}{R(s)} = \frac{K}{\tau s + 1}$$

$$R(s) = 1/s,$$

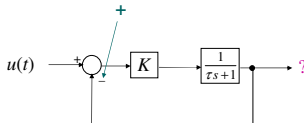
$$C(s) = \frac{1}{s} \frac{K}{\tau s + 1} = \frac{K}{s} \frac{K}{s + 1/\tau}$$

$$c(t) = K - Ke^{-t/\tau} \quad t > 0$$

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Review of Lecture 4

- What if we use positive feedback in the following closed-loop system?



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Review of Lecture 4

- What is steady-state gain (or dc gain) of a system?
- Given $G(s)$, the transfer function of a system, how to calculate its steady-state gain?

Remark: The system dc gain is the steady-state gain to a constant input for the case the output has a final value, and it is equal to the system transfer function evaluated at $s = 0$.

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Review of Lecture 4

• Second-order systems

$$G(s) = \frac{C(s)}{R(s)} = \frac{b_0}{s^2 + a_1s + a_0} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

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Review of Lecture 4

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

Is this the direction of increase or decrease of ζ ?

• Step response

Case 1: $\zeta < 1$ (underdamped)

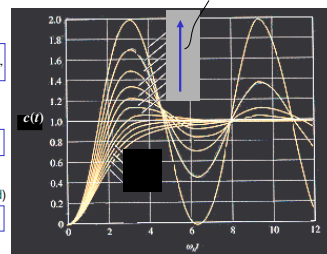
$$c(t) = 1 - \frac{1}{\beta} e^{-\zeta\omega_n t} \sin(\beta\omega_n t + \theta)$$

Case 2: $\zeta > 1$ (overdamped)

$$c(t) = 1 + k_1 e^{-t/\tau_1} + k_2 e^{-t/\tau_2}$$

Case 3: $\zeta = 1$ (critically damped)

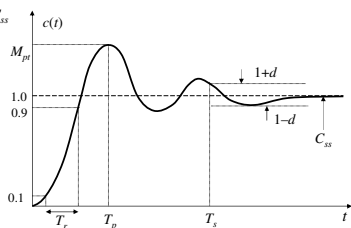
$$c(t) = 1 + k_1 e^{-t/\tau} + k_2 t e^{-t/\tau}$$



Time response of specifications in design

• Some parameters

- Rise time, T_r
- Peak value of the step response, M_p ; time to reach it, T_p (how to calculate T_p ?)
- Steady state value, C_{ss}
- Percent overshoot, $\frac{M_p - C_{ss}}{C_{ss}} \times 100$
- Settling time, T_s (how to calculate T_s ?)



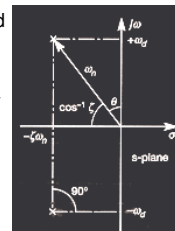
Time response of specifications in design

• Some parameters

• Time response and pole locations

- The settling time is inversely related to the real part of the poles (the speed of response is increased by moving the poles to the left in the s-plane)
- Decreasing the angle $\cos^{-1}\zeta$ (increasing ζ) reduces the percent overshoot

$$T_s = k \tau = \frac{k}{\zeta\omega_n}$$



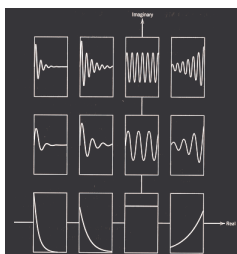
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Time response of specifications in design

• Some parameters

• Time response and pole locations

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This picture shows how changing pole locations in the s-plane affects responses

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Frequency response of systems

• Frequency response: steady-state response of systems to sinusoidal inputs

$$r(t) = A \cos \omega t, \quad R(s) = \frac{As}{s^2 + \omega_1^2}$$

Assume that $\lim_{t \rightarrow \infty} c_g(t) = 0$

$$C(s) = G(s)R(s) = \frac{k_1}{s - j\omega_1} + \frac{k_2}{s + j\omega_1} + C_g(s)$$

$$k_1 = \frac{1}{2} AG(j\omega_1), \quad k_2 = \frac{1}{2} AG(-j\omega_1), \quad G(j\omega_1) = |G(j\omega_1)| e^{j\phi(\omega_1)}$$

$$c_{ss}(t) = k_1 e^{j\omega_1 t} + k_2 e^{-j\omega_1 t} = A |G(j\omega_1)| \frac{e^{j(\omega_1 t + \phi(\omega_1))} + e^{-j(\omega_1 t + \phi(\omega_1))}}{2} = A |G(j\omega_1)| \cos(\omega_1 t + \phi(\omega_1))$$

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Frequency response of systems

- Frequency response: steady-state response of systems to sinusoidal inputs

$$r(t) = A \cos \omega_1 t, \quad G(j\omega_1) = |G(j\omega_1)| e^{j\phi(\omega_1)}$$

$$c_{ss}(t) = A |G(j\omega_1)| \cos(\omega_1 t + \phi(\omega_1))$$

- The steady-state gain of a system for a sinusoidal input is the **magnitude** of the transfer function evaluation at $s = j\omega_1$, and the **phase shift** of the output sinusoid relative to the input sinusoid is the angle of $G(j\omega_1)$

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Frequency response of systems

- Frequency response: steady-state response of systems to sinusoidal inputs

– The steady-state gain of a system for a sinusoidal input is the **magnitude** of the transfer function evaluation at $s = j\omega_1$, and the **phase shift** of the output sinusoid relative to the input sinusoid is the angle of $G(j\omega_1)$

- $G(j\omega)$ is defined as the **frequency response function**

$$G(j\omega) = |G(j\omega)| e^{j\phi(\omega)}$$

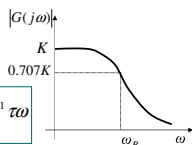
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Frequency response of systems

- Frequency response: steady-state response of systems to sinusoidal inputs
- Frequency response of first-order systems

$$G(s) = \frac{K}{\tau s + 1}$$

$$|G(j\omega)| = \frac{K}{(1 + \tau^2 \omega^2)^{1/2}}, \quad \phi(\omega) = -\tan^{-1} \tau \omega$$



- **System bandwidth**, ω_B : The frequency at which the gain is equal to $1/\sqrt{2}$ (approximately 0.707) times the gain at very low frequencies

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Frequency response of systems

- Frequency response: steady-state response of systems to sinusoidal inputs
- Frequency response of first-order systems
- Frequency response of second-order systems

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{1}{(s/\omega_n)^2 + 2\zeta(s/\omega_n) + 1}$$

$$G(j\omega) = \frac{1}{[1 - (\omega/\omega_n)^2] + j2\zeta(\omega/\omega_n)}$$

$$|G(j\omega)| = \frac{1}{\left[\left(1 - (\omega/\omega_n)^2\right)^2 + \left(2\zeta(\omega/\omega_n)\right)^2 \right]^{1/2}}$$

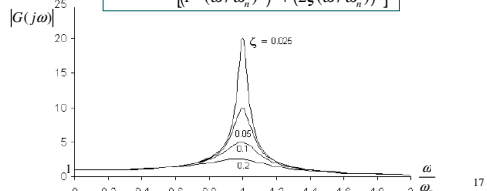
Question: What will happen if $\zeta = 0$ and $\omega = \omega_n$?

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Frequency response of systems

- Frequency response: steady-state response of systems to sinusoidal inputs
- Frequency response of first-order systems
- Frequency response of second-order systems

$$|G(j\omega)| = \frac{1}{\left[\left(1 - (\omega/\omega_n)^2\right)^2 + \left(2\zeta(\omega/\omega_n)\right)^2 \right]^{1/2}}$$



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Stability

- What do we usually mean by stability?
 - Examples of stable and unstable systems

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M2-F2 experiencing lateral oscillations in flight

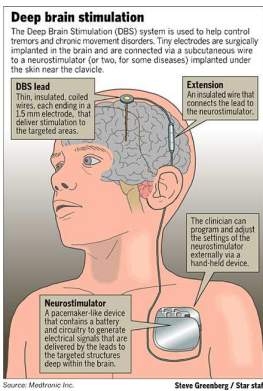
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Rest tremor in Parkinson's disease

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Deep brain stimulation for the treatment of rest tremor in Parkinson's disease

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Stability

- What do we usually mean by stability?
- **Bounded-input, bounded-output (BIBO) stability**
 - A system is BIBO stable, if, for every bounded input, the output remains bounded for all time
 - The concept of BIBO stability is not appropriate to describe stability in all nonlinear systems

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Stability

- What do we usually mean by stability?
- Bounded-input, bounded-output (BIBO) stability
- **Criteria for the BIBO stability of linear time-invariant systems**

$$R(s) \longrightarrow \boxed{T(s)} \longrightarrow C(s) \quad \boxed{T(s) = \frac{P(s)}{Q(s)}, \quad Q(s) = a_n \prod_{i=1}^n (s - p_i)}$$

$$\boxed{C(s) = T(s)R(s) = \frac{P(s)}{a_n \prod_{i=1}^n (s - p_i)} R(s) = \frac{k_1}{s - p_1} + \dots + \frac{k_n}{s - p_n} + C_r(s)}$$

– Some terms

- Characteristic equation: $Q(s) = 0$
- System roots or system poles: $p_i, i = 1, \dots, n$
- Forced response: $C_r(s)$ (the sum of terms, in the partial-fraction expansion, that originate in the poles of $R(s)$)

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Stability

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- Bounded-input, bounded-output (BIBO) stability

- **Criteria for the BIBO stability of linear time-invariant systems**

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$$C(s) = T(s)R(s) = \frac{P(s)}{a_n \prod_{i=1}^n (s - p_i)} \quad R(s) = \frac{k_1}{s - p_1} + \dots + \frac{k_n}{s - p_n} + C_r(s)$$

– Some terms

- A linear time-invariant system is BIBO stable provided all roots of the system characteristic equation (poles of the closed-loop transfer function) lie in the left half of the s -plane (why?)

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References

- C. L. Phillips and R. D. Harbor. Feedback Control Systems, 4th Edition, Prentice Hall, 2000.
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