

## Lecture 14: Bode Diagrams Examples

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## Homework 6

- Problem 8.6 (a)-(e) in the text book
- Due next Wednesday

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## About last lecture

- Three steps for general design of controllers
- Advantages and disadvantages of root-locus design
- Three ways of visualizing frequency-response function
- Definition of Bode diagram
  - Bode diagram, or Bode plot, is a plot of magnitude versus frequency and phase versus frequency with logarithmic frequency scale and magnitude scale
- Main advantage of Bode diagram

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## Outline of this lecture

- Approximate sketches of Bode diagrams
- Bode diagrams examples
  - Constant gain
  - Integrators and differentiators (poles and zeros at the origin)
  - Nonzero real poles and zeros
  - Complex poles and zeros
  - Ideal time delay
- Basic steps for constructing Bode diagrams

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## Approximate sketches of Bode diagrams

- Approximate magnitude diagram for a first-order frequency-dependent term

$$1 + j\omega / \omega_i$$

– Its magnitude in decibels equals

$$\text{dB}_i = 20 \log[1 + (\omega / \omega_i)^2]^{1/2} \quad \text{Why?}$$

$$\text{For } \omega \ll \omega_i, \text{ dB}_i \approx 0$$

Why?

$$\text{For } \omega \gg \omega_i, \text{ dB}_i \approx 20 \log \omega - 20 \log \omega_i$$

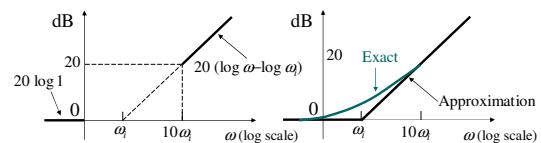
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## Approximate sketches of Bode diagrams

- Approximate magnitude diagram for a first-order frequency-dependent term

$$1 + j\omega / \omega_i, \quad \text{dB}_i = 20 \log[1 + (\omega / \omega_i)^2]^{1/2}$$

$$\text{For } \omega \ll \omega_i, \text{ dB}_i \approx 0 \quad \text{For } \omega \gg \omega_i, \text{ dB}_i \approx 20 \log \omega - 20 \log \omega_i$$



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### Approximate sketches of Bode diagrams

- Approximate magnitude diagram for a first-order frequency-dependent term
- Approximate phase diagram for a first-order frequency-dependent term

$$1 + j\omega/\omega_c$$

Its phase angle equals

$$\theta(\omega) = \tan^{-1}\left(\frac{\omega}{\omega_c}\right)$$

$$\text{For } \omega \ll \omega_c, \theta(\omega) \approx 0$$

$$\text{For } \omega \gg \omega_c, \theta(\omega) \approx 90^\circ$$

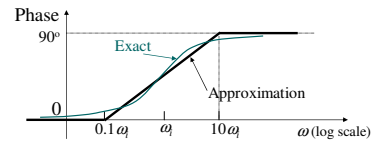
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### Approximate sketches of Bode diagrams

- Approximate magnitude diagram for a first-order frequency-dependent term
- Approximate phase diagram for a first-order frequency-dependent term

$$1 + j\omega/\omega_c, \theta(\omega) = \tan^{-1}(\omega/\omega_c)$$

$$\text{For } \omega \ll \omega_c, \theta(\omega) \approx 0 \quad \text{For } \omega \gg \omega_c, \theta(\omega) \approx 90^\circ$$



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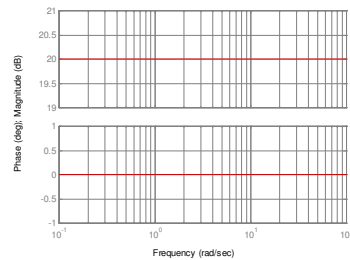
### Constant gain

Exercise 1: Sketch the Bode diagram for  $G(s) = K$ .

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### Constant gain

Constant gain  $K=10$



Questions: For what range of  $K$  does the system have positive (or negative) dB? What does the Bode diagram look like if  $K < 0$ ?

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### Poles and zeros at the origin

Exercise 1: Sketch the Bode diagram for  $G(s) = 1/s$ .

Exercise 2: Sketch the Bode diagram for  $G(s) = s$ .

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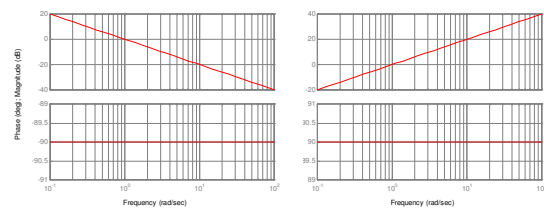
### Poles and zeros at the origin

$$G(s) = 1/s$$

Integrator

$$G(s) = s$$

Differentiator



Question 1: What are the slopes and zero-dB frequencies of the two magnitude plots?

Question 2: What if we have multiples poles or zeros at the origin?

## Nonzero real poles and zeros

**Exercise 1:** Sketch the Bode diagram for  $G(s) = 10/(s+10)$ .

**Exercise 2:** Sketch the Bode diagram for  $G(s) = (s+10)/10$ .

**Question:** What are the break frequencies (or corner frequencies) of the above systems?

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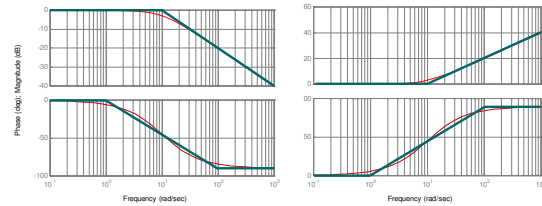
## Nonzero real poles and zeros

$$G(s) = 10/(s+10)$$

Low-pass filter

$$G(s) = (s+10)/10$$

PD controller



**Question 1:** What are the slopes of the two magnitude plots?

**Question 2:** What are the limits of the phase angles as  $\omega \rightarrow \infty$ ?

## Nonzero real poles and zeros

**Exercise 3:** Sketch the Bode diagram for  $G(s) = 10(s+1)/(s+10)$ .

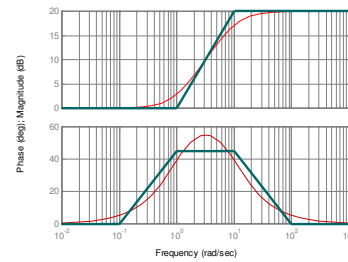
**Question:** Is this a phase-lead controller or phase-lag controller?

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## Nonzero real poles and zeros

$$G(s) = \frac{10(s+1)}{s+10}$$

Phase-lead controller



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## Complex zeros and poles

- Consider poles or zeros of the form

$$s^2 + 2\zeta\omega_n s + \omega_n^2$$

**Question:** For which range of the damping ratio do we get complex poles or zeros?

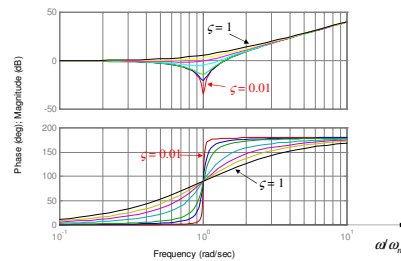
- Straight-line approximations may be very inaccurate for some value of the damping ratio (**question:** for small value or for large value?)

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## Complex zeros and poles

$$G(s) = 1 + 2\zeta \frac{s}{\omega_n} + \left(\frac{s}{\omega_n}\right)^2$$

Complex zeros



### Ideal time delay

**Exercise:** Sketch the Bode diagram for

$$G(s) = e^{-t_0 s}$$

**Question:** Can we approximate the ideal time delay with a rational function?

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### Basic steps for constructing Bode diagrams

- Step 1: Rewrite the transfer function in proper form so that the lowest order term (nonzero) in the numerator and denominator are both unity

– Examples:

$$G(s) = \frac{30(s+10)}{s^2+3s+50} = \frac{30 \cdot 10 \cdot (\frac{s}{10} + 1)}{50 \cdot (\frac{s^2}{50} + \frac{3}{50}s + 1)} = 6 \frac{\frac{s}{10} + 1}{\frac{s^2}{50} + \frac{3}{50}s + 1}$$

$$G(s) = \frac{5s}{s^2+3s+50} = \frac{5 \cdot \frac{s}{1}}{50 \cdot (\frac{s^2}{50} + \frac{3}{50}s + 1)} = \frac{1}{10} \frac{\frac{s}{1}}{\frac{s^2}{50} + \frac{3}{50}s + 1}$$

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### Basic steps for constructing Bode diagrams

- Step 1: Rewrite the transfer function in proper form so that the lowest order term (nonzero) in the numerator and denominator are both unity
- Step 2: Separate the transfer function into its constituent parts—a constant, poles and zeros at the origin, nonzero real poles and zeros, and complex conjugate poles and zeros

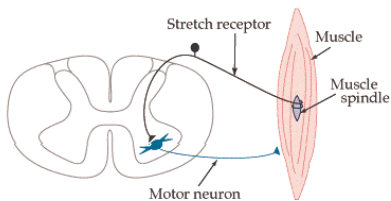
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### Basic steps for constructing Bode diagrams

- Step 1: Rewrite the transfer function in proper form so that the lowest order term (nonzero) in the numerator and denominator are both unity
- Step 2: Separate the transfer function into its constituent parts—a constant, poles and zeros at the origin, nonzero real poles and zeros, and complex conjugate poles and zeros
- Step 3: Draw the Bode diagram for each part
- Step 4: Draw the overall Bode diagram by adding up the results from Step 3

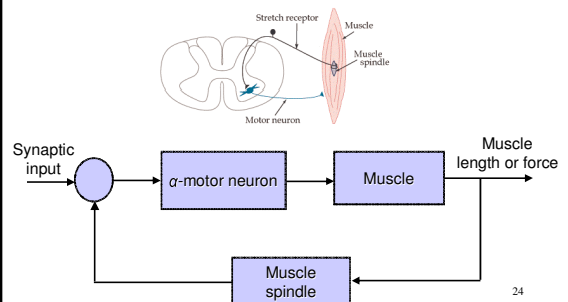
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### Monosynaptic stretch reflex: “shortest” feedback control in neural systems

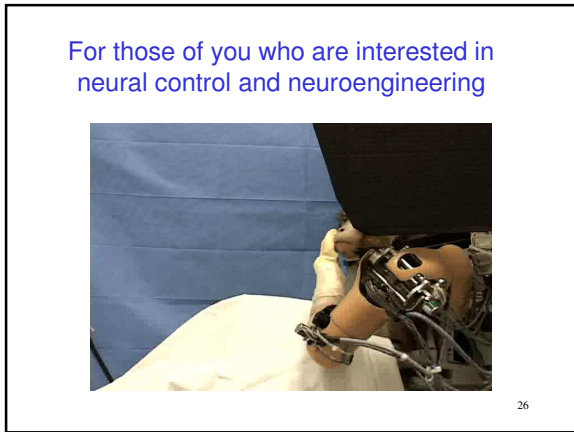
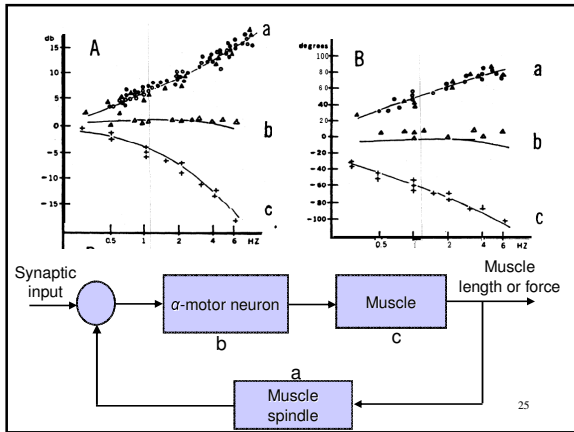


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### Monosynaptic stretch reflex: “shortest” feedback control in neural systems



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### References

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- D. Weber. Lecture notes for BioE 2696/ECE 2695 Control Theory in Neuroscience, University of Pittsburgh, Pittsburgh, PA, 2009.
- <http://motorlab.neurobio.pitt.edu/multimedia.php>